

Variation of Flux Reflected in Solar Parabolic trough **Collectors with Rim Angle**

Hamza Al-Tahaineh*1, Rebhi Damsah²⁾, and Omar AL-Zoubi³⁾

^{1,2)}Mechanical Engineering Department, Al-Huson University College, Al-Balqa Applied University, Al-Huson, 21510, Jordan. ³⁾Renewable Energy Engineering Department, Faculty of Engineering, Al al-Bayt University, P.O. Box 130040, Al-Mafraq, 25113, Jordan.

Abstract

A wide range of solar energy applications can benefit from the parabolic collector, including power generation, heating, and cooling. One of the most important parameters that affect the performance of a parabolic trough collector is its rim angle. This study examines how to rim angle affects the intensity of incoming photons reflected from the collector surface to the receiver. Flux distribution was simulated employing Ray tracing Simulation software. Out of 3000 photons employed in the experiment, 126 to 1608 photons were reflected from the collector to the receiver. A narrower rim angle results in a greater number of photons reflected per aperture width. A smaller aperture width also produces more photons for the focal length range studied. Paper type: Research paper

Keywords: rim angle; focal length; aperture width; parabolic trough collector; flux distribution.

Citation: Al-Tahaineh, H., Damsah, and O., AL-Zoubi "Variation of flux reflected in solar parabolic trough collectors with rim angle", Jordanian Journal of Engineering and Chemical Industries, Vol. 5, No.3, pp: 78-81 (2022).

Introduction

The solar parabolic trough is a concentrated collector for solar energy. The parabolic trough is used to focus low- and mediumtemperature radiation. The concentration ratio, defined as the ratio of aperture area to receiver area, of a parabolic trough is 30 to 100, with temperatures up to 400°C (Barlev et al., 2011). Depending on whether the image of the sun is concentrated on the receiver, concentrating collectors can be characterized as non-imaging or imaging. Parabolic troughs are considered a form of image concentrator (Billy et al., 2015). The thermal performance of a parabolic trough collector with absorber tube misalignment and reflector slope inaccuracy has been assessed using the finite volume approach. For 70mm diameter tubes with absorber tube dislocation, collector efficiency might fall by up to 11% in the presence of slope inaccuracy. (Ramesh et al., 2019). Investigations were conducted on a parabolic trough solar collector. The effect of collector rim angles and non-uniform heat flux distribution boundaries on the interior heat transfer coefficients of an absorber tube was investigated using numerical simulation in ANSYS. Where significant buoyancy effects existed, laminar flow steady-state conditions were considered. A user-defined function in Fluent was used to implement sine-wave non-uniform heat flux distributions and boundary conditions. It was found that the circumferential span of non-uniform heat flux allocations and the collector rim angle both increases the temperature of the absorber tube walls. (Okafor, 2020). As depicted in Figure 1, the solar collector is made up of parabolic trough-shaped reflectors and receivers. The receiver is an evacuated tube with heat fluid flowing through and is supported by metal. The line-type receiver is fixed along the focal of the reflector's parabolic cylinder. The parabolic trough reflector is allowed to track the sun with a single-axis tracking mechanism derived from an electric or hydraulic actuator. The outer surface of the concentric cylindrical receiver is glass while the inner tube is made of copper or stainless steel coated with selective dark colour and the annulus is evacuated to reduce the convective heat losses from the receiver-heated fluid (Xu et al., 2015). A parabolic trough collector's cross-section reveals several key components. When incoming radiation contacts the reflector at the collector's rim (where the mirror radius, r_{r_0} is greatest), an angle, φ_{r_0} is created with the collector's centre line. The rim angle is the name given to this angle. In terms of the coordinate system, the parabola's equation is (Sulaiman et al., 2008):

$$y^2 = 4fx$$

(1)

where f denotes the focal length defined as the distance between the vertex and the focus along the axis of symmetry and x is the depth of the parabola at its vertex.

Jordanian Journal of Engineering and Chemical Industries (JJECI), Vol.5, No.3, 2022, pp. 78-81. 0 3

^{*} Corresponding author: E-mail: h-tahaineh@bau.edu.jo Received on April 4, 2022.

Figure 2 and trigonometry may be used to determine the receiver's diameter (D) required to catch the entire solar image as illustrated by (Kalogirou et al., 1997):

$$D = 2r_r \sin \theta_m \tag{2}$$

Where θ_m is the half acceptance angle (degrees).

Receiver detail

Glass cove

Another critical parameter in the parabolic trough is the aperture width, denoted by W_a , which is proportional to the parabola's focal length and the rim angle φ_r (Kalogirou *et al.*, 1997).



Receiver tube

Fig. 1 Parabolic trough collector schematic diagram with cooper receiver (Kalogirou, 2013).

$$W_a = 4f * \tan\frac{\varphi_r}{2} \tag{3}$$

Following Kalogirou, the reflecting surface's curve length is given by (Kalogirou et al., 1997):

Sun rays

Parabola

Tracking

Receive

$$W_a = \frac{H_p}{2} \left\{ \sec\left(\frac{\vartheta_r}{2}\right) tan\left(\frac{\vartheta_r}{2}\right) + \ln\left[\sec\left(\frac{\vartheta_r}{2}\right) tan\left(\frac{\vartheta_r}{2}\right)\right] \right\}$$
(4)

Where H_p is the parabola's lactus rectum (m), *i.e.* the parabola's opening at the focal point. The collector's surface area, on the other hand, decreases as the rim angle is reduced. This means that using narrower rim angles makes sense because the loss of optical efficiency is minimal and the cost savings in reflecting material are significant (Kalogirou et al., 1997).

1 Materials and Methods 1.1 Modelling

The purpose of parabolic trough collector modelling is to demonstrate the effect of a variety of parameters on the rim angle of the trough parabola during analysis (ASHRAE, 1986). As illustrated in Figure 3, a parabolic trough is modelled using Tonatiuh's ray tracing software. Two primary parameters affect the parabolic trough: These are the aperture width (w_a) and focal length characteristics (f). Sun radiation is assumed to be perpendicular to the aperture area based on the



Fig. 3 Model of the parabolic trough in Tonatiuh (a) $(W_a=4m)$; (b) $(W_a=8m)$

coordinate set. It was determined that the reflective surface should be a perfect specular reflector with a reflectivity of one. The diameter of the receiver was adjusted to 10cm, and the material used for the receiver was chosen to be specular with a reflectivity of 0. Any sunbath can be used to model the parabolic trough. The simulation interface is used to generate the parabola. After that, the parabola is exposed to a solar collection environment with a specified transmissivity. Before initiating the simulation, the parabola's basic parameter is entered. Before performing the simulation, the parameters are also checked to ensure that the parabola is in the right condition (Joardder, et al., 2017).

1.2 Simulation ray model

For the construction and optimization of concentrated solar collector configurations such as the parabolic trough collector, ray tracing models are highly useful (Saša et al., 2015). A ray tracing approach is used in this investigation to recreate the sun's radiation within the trough parabola. The parabolic trough's aperture width is adjustable to 4, 5, 6, 7, and 8 meters. Additionally, the focal distance is varied for each run between 0.5, 1, 1.5, 2, and 2.5 meters. In any instance, after the parameters have been defined, the ray tracing begins. The incident flux at the receiver is mapped using two-dimensional coordinate mapping. The simulation seen in Figure 4 is a ray tracing simulation; each ray represents a photon of light. The reflections of each concentrator element are analytically mapped onto the cylindrical receiver's surface. The concentration on the receiver surface under idealized conditions of collimated solar



incidence parallel to the axis of a perfect-surface concentrator is calculated first. The incidence angle is set at 0 degrees. After that, a general solar radiation map is derived.

2 Results and Discussion 2.1 Focused flux distribution

The photons reflected from the concentrator to the receiver are depicted in Figure 5. The concentration ratio of the trough design can relate to the number of photons reflected on the receiver. The flux coordinate may be used to determine the flux's intensity, as shown in the diagrams below. The arrangement with the largest parabolic trough has the fewest reflected photons, especially when the focal length is 0.5 meters (128 photons); the configuration with a 4-meter aperture width and a 2-meter focal length has the most reflected photons. To determine the amount of optical concentration, count the number of photons that return from the trough collector and travel to the receiver.



Fig. 1 Ray simulation of the parabolic trough collector.



Fig. 5 Reflected flux distribution.

2.2 Solar intensity and rim angle

The intensity of incident solar radiation that is reflected is influenced by the rim angle (i.e., the number of photons reflected changes according to the different rim angles). Indeed, the size of the rim angle determines the quantity of material used to create the parabolic surface (Boultinghouse, 1982). The number of reflected photons may be used to calculate the rim angles. The rim angle and photon count for a parabolic trough with a 4-meter aperture width are shown in Table 1. The rim angle and the number of photons reflected on the receiver from the collection are shown in Figure 6.

Table 1 Rim angle, number of photons at different focal lengths for

	-		
trough	parabola	of	$W_a=4m$

<u> </u>		
Focal length (m)	Rim angle (degree)	Number of photons
0.5	126.9	324
1	90	514
1.5	67.4	1592
2	53.13	1608
2.5	43.6	454

The results obtained demonstrate that as the aperture width of the parabolic trough lowers, the quantity of photons reflected increases. Additionally, the number of photons per aperture width decreases as the rim angle increases. There is an optimal moment for each aperture width when the number of photons is greatest. For instance, for a 4 meters aperture width, the maximum number of photons occurs at a rim angle of approximately 53 degrees. As the rim angle goes down from 136 degrees to 53 degrees, the number of photons rises at each aperture width. At a rim angle of 64 degrees, there are 1261 photons.

Conclusions

The rim angle value determines the magnitude of incident solar radiation's reflected flux. Using the rim angle, you can figure out how long the parabolic trough is and how much material is needed to make the parabolic surface. A greater number of





photons are reflected per aperture width when the rim angle is narrower. A smaller aperture width generates more photons for the focal length range under consideration. Around 1700 photons were found with an aperture width of w m while 1000 for an aperture of 7m. More studies can be done to illustrate how the rim angle influences the flux intensity and efficiency of the concentrated solar collector.

Nomenclature

=receiver diameter	[m]
=focal length	[m]
=heat collection element	[-]
=parabola's lactus rectum	[m]
=mirror radius	[m]
=aperture width	[m]
=vertex-to-focus distance	[m]
=half acceptance angle	[degree]
=rim angle	[degree]
	=receiver diameter =focal length =heat collection element =parabola's lactus rectum =mirror radius =aperture width =vertex-to-focus distance =half acceptance angle =rim angle

References

ASHRAE Standard 93-1986. Methods of testing to determine the thermal performance of solar collectors. ANSI/ASHRAE 93, 1986.

Billy, A., S., Zainudin, M. F., Ali, T., Z., Abu Bakar, R., and G. L. Ming "Effect of rim angle to the flux distribution diameter in solar parabolic dish collector", *Energy Procedia*, 68, 45-52, (2015).

Boultinghouse, K., D., Technical report: Development of a Solar-Flux Tracker for Parabolic-Trough Collectors. Sandia National Laboratory, Albuquerque, NM, (1982).

Joardder, M. U. H., Halder, P. K., Rahim, M. A., and M., H., Masud "Solar Pyrolysis", Clean Energy for Sustainable Development, Academic Press, (2017).

Kalogirou, S., Lloyd, S., and J., Ward "Modelling, optimisation and performance evaluation of a parabolic trough solar collector steam generation system", Solar Energy, 60, 49-56, (1997).

Xu, L., Z. F., Wang, G., F., Yuan, F., H., Sun, and X., L., Zhang "Thermal performance of parabolic trough solar collectors under the condition of dramatically varying DNI", *Energy Procedia*, 69, 218-225, (2015).

Okafor, I., F., "Influence of Rim Angles and Heat flux Distribution Boundary on the Heat Transfer of an Absorber Tube for a Parabolic Trough Solar Collector", IOP Conf. Series: Earth and Environmental Science, **730**, (2021).

Ramesh, K., D., and S., Kumar "Thermal performance of parabolic trough collector with absorber tube misalignment and slope error", *Solar Energy*, **184**, 246-259, (2019).

Saša, R., P., and V., P., Stefanovic "Ray Tracing Study of Optical Characteristics of the Solar Image in the Receiver for a Thermal Solar Parabolic Dish Collector", J. of Solar Energy, (2015).

Sulaiman, M., Y., Bashria, A., Y., and N., M., Adam "Design of tracking system for UPM solar bowl, sustainability for future through advanced technology", Institute of Advanced Technology, Universiti Putra Malaysia; (2008).